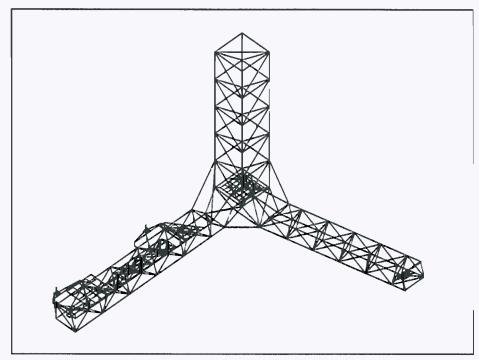


## Finite Element Geometry



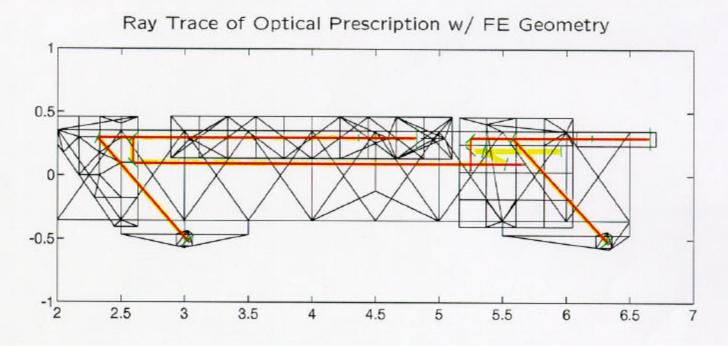
- Structural model specified in IMOS.
- Structural model consists of plate, beam, truss, and rigid body elements (RBEs).
- 2,577 total dofs: 1,832 independent w.r.t. multi-point constraints
- Experimentally determined element properties consistent with validation of modeling methodology.
- Finite element description  $(d \in \mathbb{R}^{2577})$ :

$$M\ddot{d} + Kd = B_f f$$

• Incorporation of multi-point constraints from RBEs  $(d_n \in R^{1832})$ :

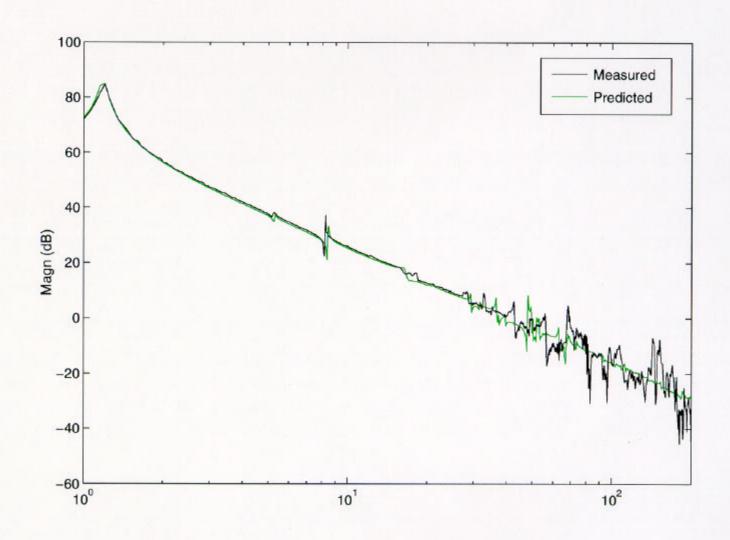
$$d = \begin{bmatrix} d_n \\ d_m \end{bmatrix} = Gd_n \implies M_{nn} \ddot{d}_n + K_{nn} d_n = B_{nf} f$$



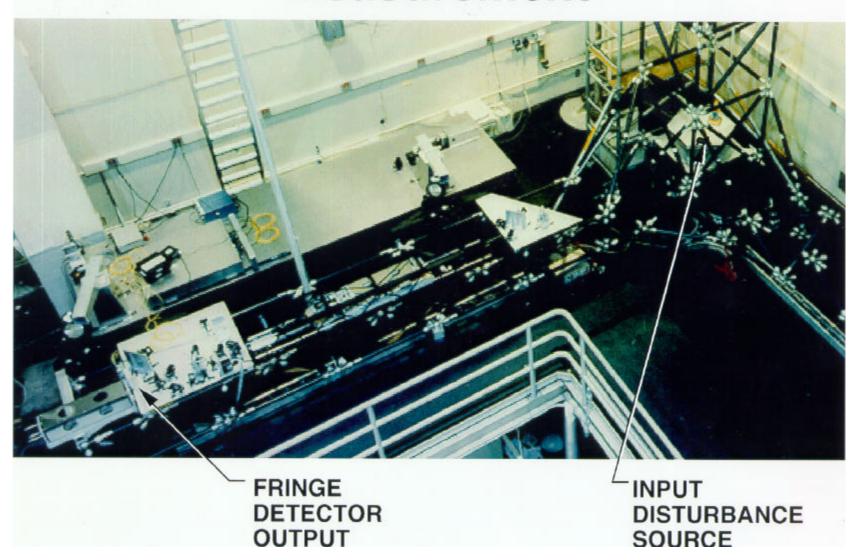


- Optical prescription specifies shapes, positions, and orientations of optical elements.
- Prescription is specified in IMOS relative to the structural model, thereby easing model integration.
- Analytic differential ray trace (COMP) yields linear optical perturbation model:

$$y_{opt} = C_{opt} d$$



## MPI Testbed Transfer Function Measurement





• Typically, disturbance has broadband PSD,  $\Phi_d(\omega)$ , and the performance measure is OPD variation,  $\sigma_{opd}$ :

$$\sigma_{opd}^2 = \frac{1}{\pi} \int_0^\infty |G(j\omega)|^2 \, \Phi_d(\omega) \, d\omega$$

- ullet Generally, an accuracy of a **factor of two** in  $\sigma_{opd}$  is desired.
- Use a bandlimited white noise disturbance to characterize the accuracy of the predicted transfer functions in the frequency range of interest  $([\omega_1, \, \omega_2])$ :

$$\sigma_g^2 = \frac{1}{\pi} \int_{\omega_1}^{\omega_2} |G(j\omega)|^2 d\omega$$

ullet Apply the factor of two desirement to the ratio of  $\sigma_g$  for the predicted and measured transfer functions:

$$\frac{1}{2} \le \frac{\sigma_{gp}}{\sigma_{gm}} \le 2$$

## INTEGRATED MODELING OF OPTICAL SYSTEMS (IMOS): CLOSED LOOP MODELING METHODOLOGY VALIDATION

